

## 2-D vector rocket equations with air drag

### 1. Burnout time

The average mass of the rocket during boost is

$$(1.1) \quad m_A = m_D + \frac{m_P}{2}$$

$m_A$  = Average mass [ kg ]

$m_D$  = Rocket dry mass [ kg ]

$m_P$  = Propellant mass [ kg ]

The coast mass is equal to the rocket dry mass.

The air drag  $F_D$  for the rocket is given by

$$(1.2) \quad F_D = k \cdot v_{t_B}^2 = \frac{1}{2} \cdot \rho \cdot C_{D_R} \cdot A_R$$

$v_{t_B}$  = Burnout velocity [  $\frac{m}{s}$  ]

$\rho$  = Air density [  $\frac{kg}{m^3}$  ]

$C_{D_R}$  = Drag coefficient of the rocket [-] (0.75 for average rockets)

$A_R$  = Rocket cross-sectional area [  $m^2$  ]

The thrust of the rocket  $F_T$  is then

$$(1.3) \quad F_T = T - m_A \cdot g - k \cdot v_{t_B}^2$$

$T$  = Motor thrust [ N ]

$g$  = Acceleration of gravity [  $\frac{m}{s^2}$  ]

The definition of force is

$$(1.4) \quad F = m \cdot a$$

As the mass is constant the factor rule in differentiation allows the mass to move outside the derivative operator, and the equation becomes

$$(1.5) F = m \cdot \frac{dv}{dt}$$

$$(1.6) m_A \cdot \frac{dv}{dt} = T - m_A \cdot g - k \cdot v^2$$

$$(1.7) m_A \cdot \frac{dv}{dt} = T - m_A \cdot g - k \cdot v^2$$

$$(1.8) dt = \frac{m_A \cdot dv}{T - m_A \cdot g - k \cdot v^2} = \frac{m_A \cdot dv}{k \cdot \frac{T - m_A \cdot g}{k} - k \cdot v^2}$$

Substituting  $x^2 = \frac{T - m_A \cdot g}{k}$  yields to

$$(1.9) dt = \frac{m_A \cdot dv}{k \cdot x^2 - k \cdot v^2} = \frac{m_A}{k} \cdot \frac{dv}{x^2 - v^2}$$

To get now the burnout time  $t_B$ , we integrate over  $v_{t_B}$

$$(1.10) t_B = \frac{m_A}{k} \cdot \int \left( \frac{1}{x^2 - v^2} \right) dv_{t_B}$$

$$(1.11) t_B = \frac{m_A}{k} \cdot \frac{\ln(x + v_{t_B}) - \ln(v_{t_B} - x)}{2x} + C$$

With the condition  $t_B = 0$  (and thus  $v_{t_B} = 0$ ) we can determine the integration constant  $C$ :

$$(1.12) \frac{m_A}{k} \cdot \frac{\ln(x) - \ln(-x)}{2x} + C = 0$$

$$(1.13) C = \frac{m_A}{k} \cdot \frac{\ln(-x) - \ln(x)}{2x}$$

(1.14)

$$t_B = \frac{m_A}{k} \cdot \frac{\ln(x + v_{t_B}) - \ln(v_{t_B} - x)}{2x} + \frac{m_A}{k} \cdot \frac{\ln(-x) - \ln(x)}{2x} = \frac{m_A}{2 \cdot k \cdot x} \cdot \left( \ln(x + v_{t_B}) - \ln(v_{t_B} - x) + \ln(-x) - \ln(x) \right)$$

(1.15)

$$t_B = \frac{m_A}{k} \cdot \frac{\ln(x + v_{t_B}) - \ln(v_{t_B} - x)}{2x} + \frac{m_A}{k} \cdot \frac{\ln(-x) - \ln(x)}{2x} = \frac{m_A}{2 \cdot k \cdot x} \cdot \left( \ln\left(\frac{x + v_{t_B}}{x}\right) + \ln\left(\frac{-x}{v_{t_B} - x}\right) \right)$$

$$(1.16) \quad t_B = \frac{m_A}{2 \cdot k \cdot x} \cdot \ln\left(\frac{x + v_{t_B}}{x - v_{t_B}}\right)$$

**Burnout time equation**

## 2. Burnout velocity

Solving now for  $v_{t_B}$  :

$$(1.17) \quad \frac{2 \cdot k \cdot x}{m_A} \cdot t_B = \ln\left(\frac{x + v_{t_B}}{x - v_{t_B}}\right)$$

$$\text{Substitution } y = \frac{2 \cdot k \cdot x}{m_A}$$

$$(1.18) \quad y \cdot t_B = \ln\left(\frac{x + v_{t_B}}{x - v_{t_B}}\right)$$

$$(1.19) \quad e^{y \cdot t_B} = \frac{x + v_{t_B}}{x - v_{t_B}}$$

$$(1.20) \quad x \cdot e^{y \cdot t_B} - x = v_{t_B} (1 + e^{y \cdot t_B})$$

$$(1.21) \quad v_{t_B} = x \cdot \frac{e^{y \cdot t_B} - 1}{e^{y \cdot t_B} + 1}$$

**Burnout velocity equation**

The burnout time  $t_B$  can be also written as

$$t_B = \frac{I_{sp}}{T} = \frac{v_e}{g \cdot T}$$

$I_{sp}$  = Specific impulse [ s ]

$v_e$  = Effective exhaust velocity [ $\frac{m}{s}$ ]

### 3. Burnout altitude

To get now the burnout velocity  $h_B$  we need to integrate 1.21 over the burnout time:

$$(1.22) \quad h_B = \int \left( x \cdot \frac{e^{y \cdot t} - 1}{e^{y \cdot t} + 1} \right) dt_B = \frac{2 \cdot x \cdot \ln(e^{y \cdot t_B} + 1) - t_B \cdot x \cdot y}{y} + C$$

$$(1.23) \quad h_B = \frac{2 \cdot x \cdot \ln(e^{y \cdot t_B} + 1) - t_B \cdot x \cdot y}{y} + C$$

With the condition  $h_B = 0$  (and thus  $t_B = 0$ ) we can determine the integration constant  $C$ :

$$(1.24) \quad \frac{2 \cdot x \cdot \ln(2)}{y} + C = 0$$

$$(1.25) \quad C = -\frac{2 \cdot x \cdot \ln(2)}{y}$$

$$(1.26) \quad h_B = \frac{2 \cdot x}{y} \cdot \ln\left(\frac{e^{y \cdot t_B} + 1}{2}\right) - t_B \cdot x$$

Substitution  $y = \frac{2 \cdot k \cdot x}{m_A}$

$$(1.27) \quad h_B = \frac{m_A}{k} \cdot \ln\left(\frac{e^{y \cdot t_B} + 1}{2}\right) - t_B \cdot x$$

**Burnout altitude equation 1**

Replacing  $e^{y \cdot t_B}$  by

$$(1.28) \quad \frac{x + v_{t_B}}{x - v_{t_B}} = e^{y \cdot t_B}$$

yields to

$$(1.29) \quad h_B = \frac{m_A}{k} \cdot \ln\left(\frac{x}{x - v_{t_B}}\right) - t_B \cdot x$$

$$(1.30) \quad t_B = \frac{m_A}{2 \cdot k \cdot x} \cdot \ln\left(\frac{x + v_{t_B}}{x - v_{t_B}}\right)$$

$$(1.31) \quad h_B = \frac{m_A}{k} \cdot \ln\left(\frac{x}{x - v_{t_B}}\right) - \left(\frac{m_A}{2 \cdot k \cdot x} \cdot \ln\left(\frac{x + v_{t_B}}{x - v_{t_B}}\right)\right) \cdot x$$

$$(1.32) \quad h_B = \frac{m_A}{k} \cdot \ln\left(\frac{x}{x - v_{t_B}}\right) - \frac{m_A}{2 \cdot k} \cdot \ln\left(\frac{x + v_{t_B}}{x - v_{t_B}}\right)$$

$$(1.33) \quad h_B = \frac{2 \cdot m_A}{2 \cdot k} \cdot \ln\left(\frac{x}{x - v_{t_B}}\right) - \frac{m_A}{2 \cdot k} \cdot \ln\left(\frac{x + v_{t_B}}{x - v_{t_B}}\right)$$

$$(1.34) \quad h_B = \frac{m_A}{2 \cdot k} \cdot \ln\left(\frac{x}{x - v_{t_B}}\right)^2 - \frac{m_A}{2 \cdot k} \cdot \ln\left(\frac{x + v_{t_B}}{x - v_{t_B}}\right)$$

$$(1.35) \quad h_B = \frac{m_A}{2 \cdot k} \cdot \ln\left(\frac{x^2}{(x - v_{t_B})^2} \cdot \frac{x - v_{t_B}}{x + v_{t_B}}\right)$$

$$(1.36) \quad h_B = \frac{m_A}{2 \cdot k} \cdot \ln\left(\frac{x^2}{x^2 - v_{t_B}^2}\right)$$

**Burnout altitude equation 2**

#### 4. Coasting altitude

After the rocket has reached the burnout altitude, the so called coasting phase begins. The rocket has then the dry mass  $m_D$  and the initial velocity  $v_{t_B}$ . To derive the coast altitude  $h_C$  we start again with the definition of force:

$$(1.37) \quad F = m \cdot a = m \cdot v \cdot \frac{dv}{dh}$$

$$(1.38) \quad m_D \cdot v \cdot \frac{dv}{dh} = -m_D \cdot g - k \cdot v^2$$

$$(1.39) \quad dh = \frac{m_D \cdot v \cdot dv}{-m_D \cdot g - k \cdot v^2}$$

$$(1.40) \quad dh = \frac{m_D \cdot v \cdot dv}{k \cdot \frac{-m_D \cdot g}{k} - k \cdot v^2}$$

Substitution  $z^2 = \frac{-m_D \cdot g}{k}$

$$(1.41) \quad dh = \frac{m_D}{k} \cdot \frac{v \cdot dv}{z^2 - v^2}$$

$$(1.42) \quad dh = \frac{m_D}{k} \cdot \frac{v \cdot dv}{z^2 - v^2}$$

$$(1.43) \quad h_C = \frac{m_D}{k} \cdot \int \left( \frac{v}{z^2 - v^2} \right) dv_{t_B}$$

$$(1.44) \quad h_C = \frac{m_D}{k} \cdot \int \left( \frac{v_{t_B}}{z^2 - v_{t_B}^2} \right) dv_{t_B} = \frac{m_D}{2 \cdot k} \cdot \ln(z^2 - v_{t_B}^2) + C$$

With the condition  $h_C = 0$  (and thus  $v_{t_B} = 0$ ) we can determine the integration constant  $C$ :

$$(1.45) \quad \frac{m_D}{2 \cdot k} \cdot \ln(z^2) + C = 0$$

$$(1.46) \quad C = -\frac{m_D}{2 \cdot k} \cdot \ln(z^2)$$

$$(1.47) \quad h_C = \frac{m_D}{2 \cdot k} \cdot \ln(z^2 - v_{t_B}^2) - \frac{m_D}{2 \cdot k} \cdot \ln(z^2)$$

$$(1.48) \quad h_C = \frac{m_D}{2 \cdot k} \cdot \ln \left( \frac{z^2 - v_{t_B}^2}{z^2} \right)$$

**Coast altitude equation**

## 5. Coast time

To determinate the time  $t_C$  from  $v_{t_B}$  to 0 (coasting time), the starting point is again the definition of force. The acceleration is here negative:

$$(1.49) F = m \cdot (-a) = m \cdot \left( -\frac{dv}{dt} \right)$$

$$(1.50) m_C \cdot \left( -\frac{dv}{dt} \right) = -m_C \cdot g - k \cdot v^2$$

$$(1.51) dt = m_C \cdot \frac{dv}{m_C \cdot g + k \cdot v^2}$$

$$(1.52) dt = m_C \cdot \frac{dv}{k \cdot \frac{m_C \cdot g}{k} + k \cdot v^2}$$

Substitution  $z_a^2 = \frac{m_C \cdot g}{k}$

$$(1.53) dt = \frac{m_C}{k} \cdot \frac{dv}{z_a^2 + v^2}$$

$$(1.54) t_C = \frac{m_C}{k} \cdot \int \left( \frac{1}{z_a^2 + v^2} \right) dv_{t_B} = \frac{m_C}{k} \cdot \frac{\arctan \left( \frac{v_{t_B}}{z_a} \right)}{z_a} + C$$

With the condition  $t_C = 0$  (and thus  $v_{t_B} = 0$ ) we can determine the integration constant  $C$ :

$$(1.55) \frac{m_C}{k} \cdot \frac{\arctan \left( \frac{0}{z_a} \right)}{z_a} + C = 0 \Rightarrow C = 0$$

$$(1.56) t_C = \frac{m_C}{k \cdot z_a} \cdot \arctan \left( \frac{v_{t_B}}{z_a} \right)$$

**Coast time equation**

## 6. Parachute size

The desired maximum decent velocity for a rocket is  $3\text{-}5 \frac{m}{s}$ . Therefore the parachute size needs to be accordingly calculated.

The maximum velocity  $v_E$  is then reached if the acceleration  $a = 0$ , hence

$$(1.57) F = m \cdot a = 0 = m_D \cdot g - \frac{1}{2} \cdot C_{D_p} \cdot \rho \cdot A_p \cdot v^2$$

$$(1.58) v_E = \sqrt{\frac{2 \cdot m_D \cdot g}{C_{D_p} \cdot \rho \cdot A_p}}$$

$C_{D_p}$  = Drag coefficient of the rocket [-] (0.75 for a flat sheet used for a parachute, or 1.5 for a true dome-shaped chute).

$A_R$  = Parachute area [ $m^2$ ]

Solving for  $A_p$ :

$$(1.59) A_p = \frac{2 \cdot m_D \cdot g}{v_E^2 \cdot C_{D_p} \cdot \rho}$$

The chute area is  $A_p = \frac{\pi \cdot D_p^2}{4}$ , so the chute diameter is

$$(1.60) D_p = \sqrt{\frac{8 \cdot m_D \cdot g}{\pi \cdot v_E^2 \cdot C_{D_p} \cdot \rho}}$$

**Parachute diameter equation**